MasterFlow 9500
Ultra-High Strength Grout
for Offshore Wind Turbine Installations
“BASF has successfully completed an extensive certification program in accordance with DNV-OS-C502 for their material MasterFlow 9500. It is considered a suitable material for use in load carrying grouted connections when applied in accordance with the approved procedures and within the stated application limitations.”

Andreas Lervik, Project Manager, DNV GL
MasterFlow 9500: Exagrout for Offshore Wind Turbine Installations

MasterFlow 9500 is an ultra-high strength and fatigue resistant cement based Exagrout for offshore wind turbine installations – making wind energy projects more durable, time-efficient and secure.

Typically MasterFlow 9500 is used in the grouted connections of wind turbine foundations, e.g. between transition piece and monopile, in steel jackets and similar.

The material has been especially formulated for large scale, pump applications:

- Grouting of wind turbine installations where excellent fatigue resistance is required.
- Grouting under very harsh offshore conditions and temperatures as low as 0 °C.
- All void filling from 25 mm to 600 mm where high strength and fatigue resistance is important.

Maintenance-free operation of wind farm

MasterFlow 9500 exhibits long term durability and guarantees a fast, secure and cost effective installation of the offshore wind farm. Wind turbines are special – their safe and durable installation largely depends on the correct design and interaction of all components. Our MasterFlow Exagrout’s high performance guarantees a long term and maintenance-free operation of the wind farm.

Product benefits at a glance:

- **High fatigue resistance**
  - Absorbing dynamic loads
- **Rapid strength gain**
  - Faster overall installation
- **Secure installation**
  - High early and final strengths
- **Cold weather**
  - Applicable at temperatures down to 0 °C, allowing for working in shorter weather windows
- **Proven high quality**
  - Validated and certified by DNV GL
- **Excellent durability**
  - Guaranteeing long term load transfer
BASF has instructed DNV GL to verify MasterFlow 9500 in accordance with the guideline DNV-OS-C502, for use in offshore wind turbine installations. Throughout the validation process, DNV GL has validated and witnessed a whole number of laboratory testing, mock-up trials and verified installation guidelines and Quality Assurance documents.

Several external, independent laboratories were used throughout the validation process, such as:
- Aalborg University DCE Laboratory, Denmark
- DNV GL’s own testing laboratory in Høvik, Norway
- Technische Universität München, Germany
- Applus, LGAI Technical Center S.A., Spain

An audit of the grout manufacturing equipment and facilities, and factory production control by representatives of DNV GL, was successfully concluded with excellent notes.

DNV GL – conclusions and recommendations

- The verification programme for MasterFlow 9500 has been successfully completed by DNV GL according to the defined scope of work
- Fatigue life has been tested and results compared with predictions for fatigue life in accordance with DNV-OS-C502 for equivalent stress conditions
- MasterFlow 9500 shows as good a performance under cyclic loading as reinforced concrete
- The ultra high modulus of elasticity may also give benefits with a stiffening effect
- The results of the mock-up test confirm the functional properties of MasterFlow 9500 and indicate that the grout is suitable for the intended applications
- MasterFlow 9500 exhibits very good pumpability and flowability over a long period of time. The grout is capable to be pumped through a 2 inch hose over 200 m length and 20 m elevation
- MasterFlow 9500 can be installed at temperatures down to 0 °C.
Excellent Strength even at Low Temperatures
Mechanical properties of MasterFlow 9500

Compressive strength
The compressive strength of MasterFlow 9500 was tested in accordance with EN 12390-3, using variable size specimens ranging from 150 × 300 mm cylinders to 75 mm cubes and 40 × 40 × 160 mm prisms. Figure 1 shows the strength measurements of MasterFlow 9500 tested at different ages using 150 × 300 mm cylinders.

Compressive strength – 150 × 300 mm cylinders

Figure 1

Flexural strength – tensile splitting
The flexural strength was measured in accordance with EN 196-1 on 40 × 40 × 160 mm prisms, while the splitting tensile strength was determined in accordance with EN 12390-5 on cylinders ø 100 × 200 mm. Results are shown in Table 1.

Table 1

<table>
<thead>
<tr>
<th>Time</th>
<th>Flexural strength (MPa)</th>
<th>Tensile splitting strength (MPa)</th>
</tr>
</thead>
<tbody>
<tr>
<td>28 days</td>
<td>18.4</td>
<td>8.6</td>
</tr>
</tbody>
</table>

Static and dynamic modulus of elasticity
The static modulus of elasticity was measured on cylinders ø 100 × 200 mm cured 28 days in water in accordance with EN 13412. Results are shown in Table 2. Dynamic modulus of elasticity at cold temperatures was measured on prisms cured in water according to the guideline for the “protection and repair of concrete structures” of the German Committee of Reinforced Concrete (Rili-SIB DAfStb). The results are plotted in Figure 2.

Dynamic modulus of elasticity

Figure 2

Table 2

<table>
<thead>
<tr>
<th>Time</th>
<th>Modulus of elasticity (GPa)</th>
<th>Poisson’s ratio</th>
</tr>
</thead>
<tbody>
<tr>
<td>28 days</td>
<td>50.9</td>
<td>0.199</td>
</tr>
</tbody>
</table>
Axial load capacity of grouted connections

A set of two concentric steel tubes – the annulus filled with MasterFlow 9500 – has been used to test the axial load capacity of the grouted connection under compression. The grouted connection has been exposed to pre-defined loads and relaxation before the compressive axial load has been increased until a first slip occurred. Thereafter the grouted connection was loaded and the axial load capacity is determined by the shear stresses. The results of the axial load capacity test are shown in Figure 3.

MasterFlow 9500 exhibits a compressive axial load capacity which is more than twice as high as for other grout materials used under similar test conditions.

Figure 3

Test results of compressive load capacity
Long Term Volume Stability
Shrinkage compensated formulation

Volume stability is of utmost importance in the long term durability of foundations in offshore wind turbine installations. Verification of the autogenous shrinkage is therefore vital in the validation of the grouting material used in offshore grouted connections.

What is autogenous shrinkage?

Autogenous shrinkage is the result of the chemical reaction between water and a cementitious material. The volume of the components before the reaction is typically larger than the volume of the end products i.e. hydrated cement (see Figure 4). Autogenous shrinkage can occur in wet conditions, in contradiction to drying shrinkage which occurs only in dry conditions.

Consequences of autogenous shrinkage

Autogenous shrinkage can result in debonding of the grout from the steel in grouted connections and consequently poor load transfer of the dynamic loads that act on the foundations in offshore wind turbine installations.

Laboratory testing

Autogenous shrinkage was measured using a method developed at Aalborg University. After mixing MasterFlow 9500, corrugated plastic tubes, approximately 410 mm long and 30 mm in diameter, were filled with the grout and then sealed by a plastic stopper in each end of the tube and placed in a temperature controlled room at 20 °C. After final set, the length of each specimen was measured as a function of time, using micrometer gauge (Figure 5).

Excellent laboratory results

Autogenous shrinkage results for MasterFlow 9500 can be found in Figure 6. Zero autogenous shrinkage is measured after approximately one year. The maximum autogenous shrinkage is only a fraction of other offshore grout materials in the market. Figure 6 also clearly shows the shrinkage compensation effect of MasterFlow 9500.

Long term measurement of autogenous shrinkage

![Figure 5](image-url)

![Figure 6](image-url)
Outstanding Fatigue Resistance
Absorbing dynamic loads

Fatigue resistance is the resistance to the progressive and localized structural damage that occurs when a material is subjected to cyclic loading. The nominal maximum stress values are less than the ultimate stress limit and may be below the yield stress limit of the material.

Occurring of fatigue

Fatigue occurs when a material is subjected to repeated loading and unloading. If the loads are above a certain threshold, microscopic cracks will begin to form. Eventually a crack will reach a critical size, and the structure will suddenly fracture. The offshore design standard DNV-OS-C502 gives design guidelines for how to take into account maximum and minimum stress levels for fatigue life predictions (see Figure 7).

Fatigue according DNV-OS-C502

Figure 7

Let the numbers do the talking

Fatigue calculations are made according to the formulation

\[
\log_{10} N = C_1 \cdot \left( 1 - \frac{\sigma_{\text{max}}}{C_5 \cdot f_{\text{eq}}} \right) \left( 1 - \frac{\sigma_{\text{min}}}{C_5 \cdot f_{\text{eq}}} \right)
\]

where:

- \( C_1 = 12 \) for structures in air
- \( C_1 = 10 \) for structures in water, and stress blocks having variation in the compression-compression range
- \( C_1 = 8 \) for structures in water, and stress blocks having variation in the compression-tension range
- \( \sigma_{\text{max}} = \) the numerically largest compressive stress, calculated as average within each stress-block
- \( \sigma_{\text{min}} = \) the numerically lowest compressive stress, calculated as average within each stress-block (for tension = 0)
- \( C_5 = \) strength reduction factor for the specific grout. \( C_5 = 0.85 \) shall be taken for MasterFlow 9500
Measurements under cyclic loading

The behavior of MasterFlow 9500 under cyclic loading was studied using cylindrical specimens, 60 mm in diameter and 120 mm high. The grout material has been tested for fatigue resistance in air and in water. Tests conducted in air were performed at high frequency (10 Hz), while tests in water were conducted at low frequency (0.35 Hz) in order to simulate the effect of wave actions on the foundations of offshore wind turbines (see also Figure 8).

Fatigue resistance in air and in water

Figure 8

Results as good as for reinforced concrete

The observed number of cycles to failure in the tests under cyclic loading corresponds well with the prediction according to DNV-OS-C502 (Figure 9). It can be concluded that MasterFlow 9500 shows a performance under cyclic loading that is as good as for reinforced concrete. Based on the tests, it is concluded that the design for fatigue can be carried out using formulations for fatigue life prediction in DNV-OS-C502 for reinforced concrete.

Fatigue life prediction

Figure 9
Our reference in the Irish Sea (United Kingdom) – West of Duddon Sands: 108 turbines, installed on monopile transition piece foundations. Foundation installation and grouting in a record time of just 6 months © FoundOcean Ltd
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